

# PATENT ABSTRACTS OF JAPAN

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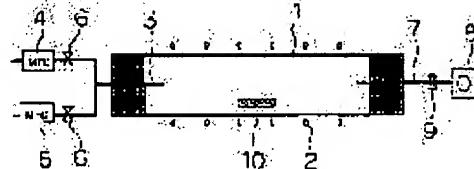
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**(54) VACUUM CARBURIZING METHOD FOR STEEL MATERIAL****(57) Abstract:**

**PROBLEM TO BE SOLVED:** To improve a defect that a treatment method using propane gas can not uniformly carburize a steel material with unopen hole or unevenness, and that a treatment method using acetylene gas or ethylene gas needs a large quantity of expansive acetylene gas and ethylene gas, though conventionally there have been a method of treating the steel material in propane gas at a pressure of 1 kPa or less, and a method of treating it in ethylene gas and acetylene gas at a pressure of 10 kPa or less, in order to prevent generation of soot, in a vacuum carburizing method of a steel material.

**SOLUTION:** This carburizing method comprises, employing mixed gas of propane and acetylene gas for the carburizing gas and making a pressure in the heating furnace in a vacuum condition of 0.05-3 kPa. It further comprises introducing the carburizing gas into the heating furnace in a pulsed way. Alternatively, it comprises introducing a certain quantity of the propane gas consecutively into the heating furnace, and introducing the acetylene gas in the pulsed way, when introducing the above carburizing gas into the heating furnace. A ratio of acetylene gas to the mixed gas is 5% or more but 50% or less.

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**CLAIMS**

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**[Claim(s)]**

[Claim 1] The vacuum carburization approach of the ferrous material characterized by performing carburization processing by setting the pressure in the above-mentioned heating furnace to 0.05-3kPa while using a liquefied petroleum gas and acetylene gas as the above-mentioned gas for carburization in the vacuum carburization approach of performing carburization processing, supplying the gas for carburization in the above-mentioned heating furnace, and adjusting gas pressure while heating a ferrous material within a heating furnace.

[Claim 2] The vacuum carburization approach of the ferrous material according to claim 1 which the above-mentioned gas for carburization is the mixed gas of the above-mentioned liquefied petroleum gas and the above-mentioned acetylene gas, and is characterized by introducing the above-mentioned mixed gas in the shape of a pulse in a heating furnace.

[Claim 3] The vacuum carburization approach of the ferrous material according to claim 1 which carries out quantum installation of the above-mentioned liquefied petroleum gas into the above-mentioned heating furnace, and is characterized by introducing the above-mentioned acetylene gas in the shape of a pulse in the above-mentioned heating furnace.

[Claim 4] The vacuum carburization approach of the ferrous material according to claim 3 characterized by introducing the above-mentioned liquefied petroleum gas into the above-mentioned heating furnace in the shape of a pulse.

[Claim 5] The vacuum carburization approach of the ferrous material according to claim 1 which carries out quantum installation of the above-mentioned acetylene gas into the above-mentioned heating furnace, and is characterized by introducing the above-mentioned liquefied petroleum gas in the shape of a pulse in the above-mentioned heating furnace.

[Claim 6] The vacuum carburization approach of a ferrous material according to claim 1, 2, 3, 4, or 5 that the ratio of the acetylene gas to the above-mentioned gas for carburization is characterized by being 50% or less 5% or more.

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**DETAILED DESCRIPTION**

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**[Detailed Description of the Invention]****[0001]**

**[Field of the Invention]** This invention relates to the vacuum carburization approach of a ferrous material, especially the vacuum carburization approach of a ferrous material of having used a liquefied petroleum gas and acetylene gas as gas for carburization.

**[0002]**

**[Description of the Prior Art]** Gas carburizing, vacuum carburization, plasma carburization, etc. are carried out to the carburization of a ferrous material from the former. Although gas carburizing is performed widely now, there are troubles, like the danger of gas combustion, grain boundary oxidation of a processing article front face, and the formation of a short cycle by high temperature carburizing are difficult. Moreover, cost is high and plasma carburization is limited to special carburization. Although processed by the pressure of 900-1100 degrees C and 10-70kPa in vacuum carburization, using saturated hydrocarbon (methane, a liquefied petroleum gas, commercial butane) as gas for carburization, for performing uniform carburization, since there was much generating of soot, time amount and costs started the maintenance in a furnace, and it did not spread other than the particular application.

**[0003]** Then, there are the approach of using a liquefied petroleum gas and processing by the pressure of 1 or less kPa, in order to control generating of soot, an approach of processing by the pressure of 1 or less kPa using acetylene gas like a thing given in JP,8-325701,A, and the approach of processing within the limits of the pressure of 1-10kPa using the mixed gas of ethylene gas and acetylene gas like a thing given in JP,2000-1765,A.

**[0004]**

**[Problem(s) to be Solved by the Invention]** However, in the art using a liquefied petroleum gas, as it had the non-through tube, the irregular ferrous material was difficult to carburize to homogeneity.

**[0005]** Moreover, in the art using acetylene gas or ethylene gas, acetylene gas and ethylene gas are expensive.

**[0006]** This invention tends to solve the above points.

**[0007]**

**[Means for Solving the Problem]** While the vacuum carburization approach of the ferrous material of this invention heats a ferrous material within a heating furnace In the vacuum carburization approach of performing carburization processing while supplying the gas for carburization in the above-mentioned heating furnace and adjusting gas pressure By using a liquefied petroleum gas and acetylene gas collectively as the above-mentioned gas for carburization It is characterized by being made by finding out that an irregular ferrous material can be carburized to homogeneity so that it may have a non-through tube, and performing carburization processing by setting the pressure in the above-mentioned heating furnace to 0.05-3kPa.

**[0008]** Moreover, the vacuum carburization approach of the ferrous material of this invention is characterized by introducing the above-mentioned mixed gas in the shape of a pulse in a heating furnace, using the mixed gas of the above-mentioned liquefied petroleum gas and the above-mentioned acetylene gas as the above-mentioned gas for carburization. Introducing in the shape of a pulse means changing a flow rate periodically in this case.

**[0009]** Moreover, the method of introducing the above-mentioned gas for carburization may carry out quantum installation of the above-mentioned liquefied petroleum gas into the above-mentioned heating furnace, may introduce the above-mentioned acetylene gas in the shape of a pulse in the above-mentioned heating furnace, and conversely, may carry out quantum installation of the above-mentioned acetylene gas

into the above-mentioned heating furnace, and may introduce the above-mentioned liquefied petroleum gas in the shape of a pulse in the above-mentioned heating furnace.

[0010] Furthermore, the method of introducing the above-mentioned gas for carburization may introduce the above-mentioned liquefied petroleum gas and the above-mentioned acetylene gas in the shape of a pulse in the above-mentioned heating furnace.

[0011] Moreover, the ratio of acetylene gas [ as opposed to the above-mentioned gas for carburization in the vacuum carburization approach of the ferrous material of this invention ] is characterized by being 50% or less 5% or more.

[0012]

[Embodiment of the Invention] With reference to a drawing, the example of this invention is explained below.

[0013] A heating furnace for 1 to carburize a ferrous material by the vacuum carburization approach of the ferrous material of this invention in drawing 1, The heater which prepared 2 in the periphery of the above-mentioned heating furnace 1, gas installation tubing the interior was made to penetrate from the heating furnace exterior which prepared 3 in the end section of the above-mentioned heating furnace 1, The acetylene gas source of supply which connected 4 to the above-mentioned gas installation tubing 3 through the bulb 6, The liquefied-petroleum-gas source of supply which similarly connected 5 to the above-mentioned gas installation tubing 3 through the bulb 6, The gas exhaust pipe which prepared 7 in the other end of the above-mentioned heating furnace 1, the vacuum exhaust which connected 8 to the above-mentioned gas exhaust pipe 7 through the adjustable exhaust air bulb 9, and 10 are ferrous materials which have the non-through tube 11 installed in the above-mentioned heating furnace 1.

[0014] (Example 1)

[0015] The quality of the material to the round bar with SCM420, an outer diameter [ of 20mm ], and a die length of 40mm The diameter of 5mm, The ferrous material 10 in which the non-through tube 11 with a depth of 37mm was formed is arranged in the center of a heating furnace 1 so that opening of the above-mentioned sheep through tube 11 may turn to the inlet of the gas installation tubing 3. It exhausted until the inside of the above-mentioned heating furnace 1 was set to 0.05 or less kPas with the above-mentioned vacuum exhaust 8, where it shut the two above-mentioned bulbs 6 and the above-mentioned adjustable exhaust air bulb 9 is made full open, and the above-mentioned ferrous material 10 was heated at 950 degrees C at homogeneity.

[0016] Then, the above-mentioned bulb 6 was opened respectively, and adjusting the exhaust air bulb 9 so that the pressure in a heating furnace 1 may grow into 2kPa(s), the liquefied petroleum gas was supplied by 40 cc/min, acetylene gas was supplied for 30 minutes by 10 cc/min, and it carburized. Then, while opening the exhaust air bulb 9 fully so that the pressure in a heating furnace 1 might be set to 0.05 or less kPas, supply of carburization gas was suspended. Furthermore heating of a heating furnace 1 was suspended, the heat insulator (not shown) was removed from the heating furnace 1, and it cooled at 160 degrees C or less.

[0017] The measurement result of the total carburization depth to the depth of a non-through tube is shown in drawing 3. It was able to carburize to the deep location of a hole rather than it carburized with a liquefied-petroleum-gas simple substance so that clearly from drawing 3.

[0018] (Example 2)

[0019] It is made the same. The quality of the material to the round bar with SCM420, an outer diameter [ of 20mm ], and a die length of 40mm The diameter of 5mm, Adjusting the exhaust air bulb 9 so that the pressure in a heating furnace 1 may be set to 0.4kPa(s), after arranging the ferrous material 10 in which the non-through tube 11 with a depth of 37mm was formed, in the heating furnace 1 center and heating a heating furnace 1 at 950 degrees C at homogeneity The liquefied petroleum gas was supplied by 90 cc/min, acetylene gas was supplied for 30 minutes by 10 cc/min, and it carburized. Then, while opening the exhaust air bulb 9 fully so that the pressure in a heating furnace 1 might be set to 0.05 or less kPas, supply of carburization gas was suspended. Furthermore heating of a heating furnace 1 was suspended, the heat insulator (not shown) was removed from the heating furnace 1, and it cooled at 160 degrees C or less. The measurement result of the total carburization depth to the depth of a non-through tube is shown in the continuous line of drawing 4.

[0020] In order to perform processing equivalent to the above-mentioned carburization result with a liquefied-petroleum-gas simple substance, as shown in the chain line of drawing 4, the flow rate of 200 cc/min is required, and since vacuum pump capacity becomes large, there is a problem that facility cost increases.

[0021] Moreover, making [ many ] a liquefied-petroleum-gas flow rate leads to making [ many ] exhaust

gas. On the other hand, if this invention approach is used, rather than the case where it carburizes with a liquefied-petroleum-gas simple substance, vacuum pump capacity can be made small and facility cost and a maintenance cost can be reduced. Moreover, a liquefied-petroleum-gas flow rate, i.e., the amount used, can be reduced.

[0022] In addition, the pressure in the above-mentioned heating furnace 1 becomes insufficient [ 0.05 or less kPas / carburization ], and generating of soot increases in 3 or more kPas.

[0023] Moreover, as for the ratio of the acetylene gas in the mixed gas of a liquefied petroleum gas and acetylene gas, at 5% or less, it is desirable for it to be ineffective and to consider as 50% or less from a cost side.

[0024] Furthermore, in case the mixed gas of a liquefied petroleum gas and acetylene gas is introduced in a heating furnace 1, installation and a halt of the above-mentioned mixed gas are repeated, and you may make it introduce the above-mentioned mixed gas in the shape of a pulse in a heating furnace 1, and carrying out the quantum style of the above-mentioned liquefied petroleum gas is continued, and you may make it add acetylene gas in pulse on the other hand again.

[0025] Moreover, the above-mentioned acetylene gas is quantitatively introduced in the above-mentioned heating furnace, you may make it add the above-mentioned liquefied petroleum gas in pulse conversely, and the above-mentioned liquefied petroleum gas and the above-mentioned acetylene gas may be further introduced in the shape of a pulse in the above-mentioned heating furnace. If it does in this way, carburization can be carried out more to homogeneity.

[0026]

[Effect of the Invention] According to the vacuum carburization approach of the ferrous material of this invention, there are big profits that the ferrous material which controls generating of soot and is irregular can be carburized to homogeneity, as mentioned above by adjusting the amount of the liquefied petroleum gas used, and the amount of expensive acetylene gas or the ethylene gas used to a liquefied petroleum gas as gas for carburization by using the gas which added acetylene gas.

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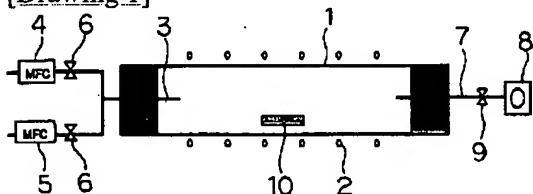
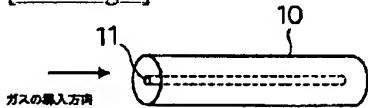
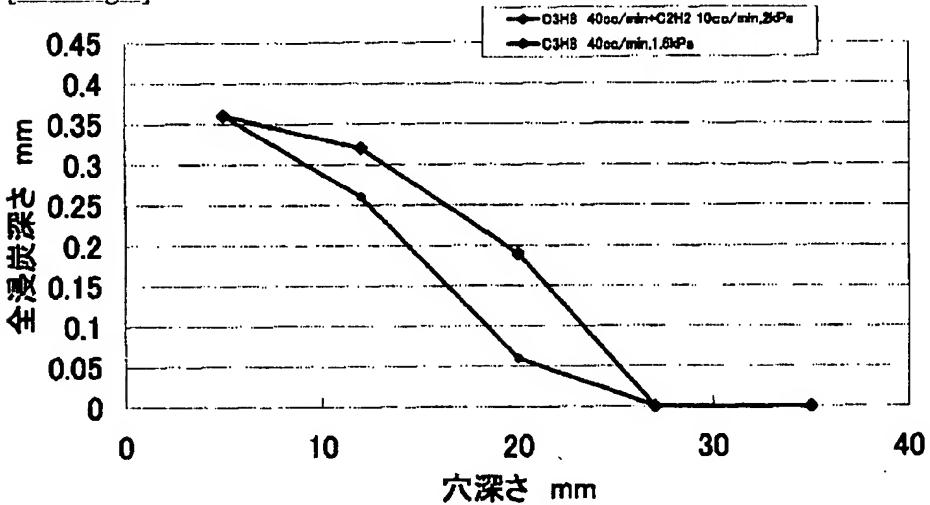
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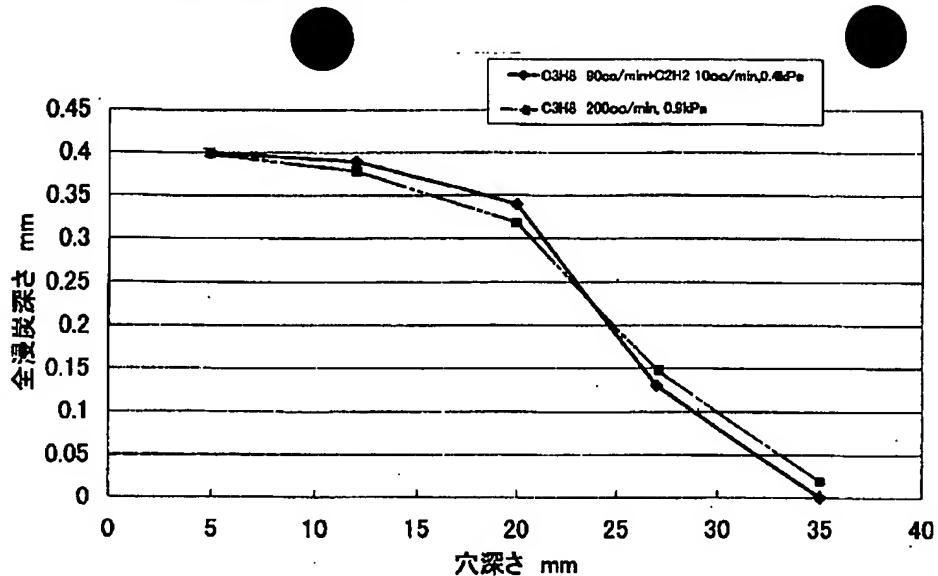
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**DRAWINGS**

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**[Drawing 1]****[Drawing 2]****[Drawing 3]****[Drawing 4]**



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[Translation done.]

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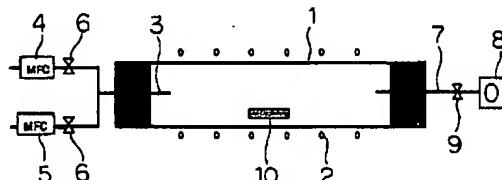
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(54)【発明の名称】 鉄鋼材料の真空浸炭方法

(57)【要約】

【課題】 従来の鉄鋼材料の真空浸炭においては、煤の発生を抑制するためにプロパンガスを用いて1kPa以下の圧力で処理する方法や、エチレンガスやアセチレンガスを用いて10kPa以下の圧力で処理する方法があったが、プロパンガスを用いた処理方法では未貫通孔のある、または凹凸のある鉄鋼材料を均一に浸炭できず、アセチレンガスやエチレンガスを用いた処理方法では高価なアセチレンガスやエチレンガスを多量に用いる必要があるという欠点があった。

【解決手段】 本発明においては、上記浸炭用ガスとしてプロパンガスとアセチレンガスの混合ガスを使用するとともに、上記加熱炉内の圧力を0.05~3kPaの真空状態として浸炭処理を行う。また、上記浸炭ガスを加熱炉内にパルス状に導入する。また、上記加熱炉内に浸炭ガスを導入することにおいて、上記プロパンガスを上記加熱炉内に定量導入し、上記アセチレンガスを上記加熱炉内にパルス状に導入する。上記混合ガスに対するアセチレンガスの比率が5%以上50%以下である。



**【特許請求の範囲】**

**【請求項1】** 鉄鋼材料を加熱炉内で加熱するとともに、上記加熱炉内に浸炭用ガスを供給し、ガス圧力を調整しながら浸炭処理を行う真空浸炭方法において、上記浸炭用ガスとしてプロパンガスとアセチレンガスを使用するとともに、上記加熱炉内の圧力を0.05～3kPaとして浸炭処理を行うことを特徴とする鉄鋼材料の真空浸炭方法。

**【請求項2】** 上記浸炭用ガスが上記プロパンガスと上記アセチレンガスの混合ガスであり、上記混合ガスを加熱炉内にパルス状に導入することを特徴とする請求項1記載の鉄鋼材料の真空浸炭方法。

**【請求項3】** 上記プロパンガスを上記加熱炉内に定量導入し、上記アセチレンガスを上記加熱炉内にパルス状に導入することを特徴とする請求項1記載の鉄鋼材料の真空浸炭方法。

**【請求項4】** 上記プロパンガスを上記加熱炉にパルス状に導入することを特徴とする請求項3記載の鉄鋼材料の真空浸炭方法。

**【請求項5】** 上記アセチレンガスを上記加熱炉内に定量導入し、上記プロパンガスを上記加熱炉内にパルス状に導入することを特徴とする請求項1記載の鉄鋼材料の真空浸炭方法。

**【請求項6】** 上記浸炭用ガスに対するアセチレンガスの比率が5%以上50%以下であることを特徴とする請求項1、2、3、4または5記載の鉄鋼材料の真空浸炭方法。

**【発明の詳細な説明】**

**【0001】**

**【発明の属する技術分野】** 本発明は鉄鋼材料の真空浸炭方法、特に浸炭用ガスとしてプロパンガスとアセチレンガスを用いた鉄鋼材料の真空浸炭方法に関するものである。

**【0002】**

**【従来の技術】** 鉄鋼材料の浸炭には従来からガス浸炭、真空浸炭、プラズマ浸炭等が行われている。ガス浸炭は現在広く行なわれているが、ガス燃焼の危険性、処理品表面の粒界酸化、高温浸炭による短サイクル化が難しい等の問題点がある。またプラズマ浸炭はコストが高く特殊浸炭に限定されている。真空浸炭では浸炭用ガスとして飽和炭化水素（メタンガス、プロパンガス、ブタンガス）を用いて900～1100°C、10～70kPaの圧力で処理するが、均一な浸炭を行うには煤の発生が多いため炉内メンテナンスに時間と費用がかかり、特殊用途以外には広がらなかつた。

**【0003】** そこで、煤の発生を抑制するためにプロパンガスを用いて1kPa以下の圧力で処理する方法や、特開平8-325701号公報記載のもののようにアセチレンガスを用いて1kPa以下の圧力で処理する方法や、特開2000-1765号公報記載のもののようにエチレンガスとアセチレンガスとの混合ガスを用いて1～10kPaの圧力の範囲内で処理する方法がある。

**【0004】**

**【発明が解決しようとする課題】** 然しながら、プロパンガスを用いた処理方法では、未貫通孔を有するような、または凹凸のある鉄鋼材料は均一に浸炭することが困難であった。

**【0005】** また、アセチレンガスやエチレンガスを用いた処理方法では、アセチレンガスやエチレンガスが高価である。

**【0006】** 本発明は上記のような点を解決しようとしたものである。

**【0007】**

**【課題を解決するための手段】** 本発明の鉄鋼材料の真空浸炭方法は、鉄鋼材料を加熱炉内で加熱するとともに、上記加熱炉内に浸炭用ガスを供給し、ガス圧力を調整しながら浸炭処理を行う真空浸炭方法において、上記浸炭用ガスとしてプロパンガスとアセチレンガスを併せて使用することにより、未貫通孔を有するような、または凹凸のある鉄鋼材料を均一に浸炭できることを見い出すことによってなされたものであり、上記加熱炉内の圧力を0.05～3kPaとして浸炭処理を行うことを特徴とする。

**【0008】** また、本発明の鉄鋼材料の真空浸炭方法は、上記浸炭用ガスとして上記プロパンガスと上記アセチレンガスの混合ガスを用い、上記混合ガスを加熱炉内にパルス状に導入することを特徴とする。パルス状に導入するというのはこの場合、周期的に流量を変化させることを意味する。

**【0009】** また、上記浸炭用ガスの導入法は上記プロパンガスを上記加熱炉内に定量導入し、上記アセチレンガスを上記加熱炉内にパルス状に導入してもよく、また逆に、上記アセチレンガスを上記加熱炉内に定量導入し、上記プロパンガスを上記加熱炉内にパルス状に導入してもよい。

**【0010】** 更に、上記浸炭用ガスの導入法は上記プロパンガス、上記アセチレンガスともに上記加熱炉内にパルス状に導入してもよい。

**【0011】** また、本発明の鉄鋼材料の真空浸炭方法は、上記浸炭用ガスに対するアセチレンガスの比率が5%以上50%以下であることを特徴とする。

**【0012】**

**【発明の実施の形態】** 以下図面を参照して本発明の実施例を説明する。

**【0013】** 図1において、1は本発明の鉄鋼材料の真空浸炭方法によって鉄鋼材料を浸炭するための加熱炉、2は上記加熱炉1の外周に設けたヒータ、3は上記加熱炉1の一端部に設けた加熱炉外部から内部に貫通せしめたガス導入管、4は上記ガス導入管3にバルブ6を介して接続したアセチレンガス供給源、5は同じく上記ガス導入管3にバルブ6を介して接続したプロパンガス供給

源、7は上記加熱炉1の他端部に設けたガス排出管、8は上記ガス排出管7に可変排気バルブ9を介して接続した真空排出装置、10は上記加熱炉1内に設置した未貫通孔11を有する鉄鋼材料である。

【0014】(実施例1)

【0015】材質がSCM420、外径20mm、長さ40mmの丸棒に直径5mm、深さ37mmの未貫通孔11を形成した鉄鋼材料10を上記未貫通孔11の開口がガス導入管3の導入口を向くよう加熱炉1の中央に配置し、上記2つのバルブ6を閉め上記可変排気バルブ9を全開にした状態で上記真空排出装置8により上記加熱炉1内が0.05kPa以下となるまで排気し、上記鉄鋼材料10を950℃に均一に加熱した。

【0016】その後、上記バルブ6を各々開き、加熱炉1内の圧力が2kPaに成るように排気バルブ9を調整しながら、プロパンガスを40cc/min、アセチレンガスを10cc/minで30分間供給して浸炭した。その後、加熱炉1内の圧力が0.05kPa以下になるように排気バルブ9を全開するとともに、浸炭ガスの供給を停止した。さらに加熱炉1の加熱を停止し、加熱炉1から断熱材(図示せず)を外して160℃以下に冷却した。

【0017】未貫通孔の深さに対する全浸炭深さの測定結果を図3に示す。図3から明らかなようにプロパンガス単体で浸炭するよりも孔の深い位置まで浸炭することができた。

【0018】(実施例2)

【0019】同様にして材質がSCM420、外径20mm、長さ40mmの丸棒に直径5mm、深さ37mmの未貫通孔11を形成した鉄鋼材料10を加熱炉1中央に配置し、加熱炉1を950℃に均一に加熱した後、加熱炉1内の圧力が0.4kPaになるように排気バルブ9を調整しながら、プロパンガスを90cc/min、アセチレンガスを10cc/minで30分間供給して浸炭した。その後、加熱炉1内の圧力が0.05kPa以下になるように排気バルブ9を全開するとともに、浸炭ガスの供給を停止した。さらに加熱炉1の加熱を停止し、加熱炉1から断熱材(図示せず)を外して160℃以下に冷却した。未貫通孔の深さに対する全浸炭深さの測定結果を図4の実線に示す。

【0020】プロパンガス単体で上記の浸炭結果と同等な処理を行なうには、図4の鎖線に示すように200cc/minもの流量が必要であり真空ポンプ容量が大きくなるので設備コストが増加するという問題がある。

【0021】また、プロパンガス流量を多くすることは排ガスを多くすることにつながる。これに対し、本発明方法を用いれば、プロパンガス単体で浸炭する場合よりも真空ポンプ容量を小さくすることができ、設備コストやメンテナンスコストを削減することができる。またプロパンガス流量、即ち使用量も減らすことができる。

【0022】なお、上記加熱炉1内の圧力が0.05kPa以下では浸炭が不十分となり、3kPa以上では煤の発生が多くなる。

【0023】また、プロパンガスとアセチレンガスの混合ガスにおけるアセチレンガスの比率は5%以下では効果がなくコスト面から50%以下とするのが好ましい。

【0024】更に、また、プロパンガスとアセチレンガスの混合ガスを加熱炉1内に導入する際には、上記混合ガスの導入と停止を繰り返して、上記混合ガスを加熱炉1内にパルス状に導入するようにもよく、また上記プロパンガスを定量流し続け、一方アセチレンガスをパルス的に加えるようにしてもよい。

【0025】また、逆に、上記アセチレンガスを上記加熱炉内に定量的に導入し、上記プロパンガスをパルス的に加えるようにしてもよいし、更に、上記プロパンガス、上記アセチレンガスとともに上記加熱炉内にパルス状に導入してもよい。このようにすれば浸炭をより均一に行なうことができる。

【0026】

【発明の効果】上記のように本発明の鉄鋼材料の真空浸炭方法によれば、浸炭用ガスとしてプロパンガスにアセチレンガスを添加したガスを用いることで、プロパンガスの使用量と高価なアセチレンガスやエチレンガスの使用量を調整することによって煤の発生を抑制して凹凸のある鉄鋼材料を均一に浸炭することができるという大きな利益がある。

【図面の簡単な説明】

【図1】本発明の真空浸炭方法に用いる加熱炉の縦断側面図である。

【図2】本発明の真空浸炭方法に用いる鉄鋼材料の斜視図である。

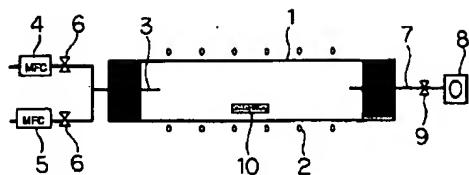
【図3】本発明の真空浸炭方法を用いて鉄鋼材料を浸炭した浸炭深さを示すグラフである。

【図4】本発明の真空浸炭方法を用いて鉄鋼材料を浸炭した浸炭深さを示すグラフである。

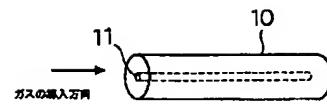
【符号の説明】

- 1 加熱炉
- 2 ヒータ
- 3 ガス導入管
- 4 アセチレンガス供給源
- 5 プロパンガス供給源
- 6 バルブ
- 7 ガス排出管
- 8 真空排出装置
- 9 可変排気バルブ
- 10 鉄鋼材料
- 11 未貫通孔

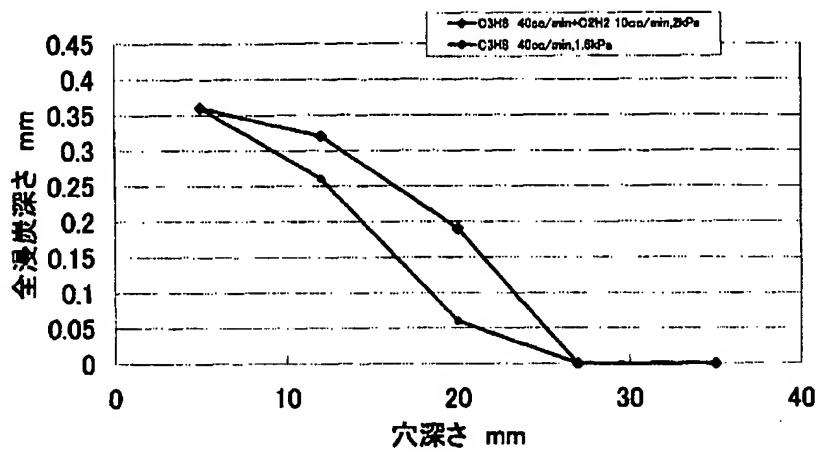
【図1】



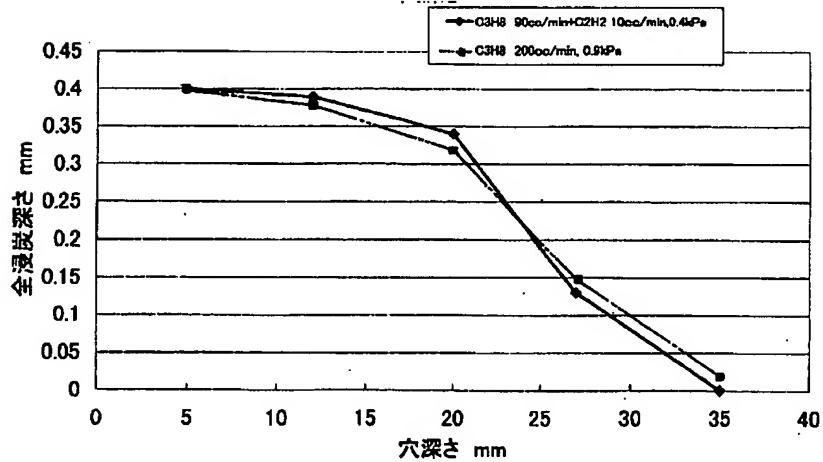
【図2】



【図3】



【図4】



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